## Wide Field Imaging

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## Introduction

- Aperture Synthesis technique first developed for radio astronomy (one resolved point per antenna)
- Optical telescopes have the advantage of a wide Field Of View (FOV)
-It is useful to keep this advantage for observation of extended or multiple objects


Telescopes A1 and A2 collect the light coming from a distant stellar source in the direction s. But the light "arrives" at the telescopes with a time difference

$$
\tau=\frac{\vec{B} \cdot \vec{s}}{c}
$$

To detect interference fringes we have to make $\tau \cdot c<L_{c}$ where $L_{c}$ is the coherent length and $\tau * \mathrm{c}$ is called the Optical Path Difference (OPD). This OPD is corrected using a delay line. When OPD $>\mathrm{L}_{\mathrm{c}}$ no interference : Narrow coherent field

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## Dual-feed technique

Separates the fields of two stars and sends each wavefront to a different delay line.
Useful for fringe acquisition/tracking on a nearby strong source.
But separating the wavefronts we lose light.

## New approach

$\vec{B}$ baseline vector
$\vec{s}$ pointing vector
$O P D=\vec{B} \cdot \vec{s}$


$$
\Delta O P D=\vec{B} \cdot\left(\vec{s}^{\prime}-\vec{s}\right)
$$

$O P D^{\prime}=\vec{B} \cdot \vec{s}^{\prime}$
If we compensate the $\triangle \mathrm{OPD}$ as function of the field angle:
Wide field of view

## Field-Angle Dependence of the $\Delta \mathbf{O P D}$

(E,A) pointing vector coordinates
( $B_{x}, B_{y}$ ) baseline coordinates
( $\mathrm{E}+\delta \mathrm{E}, \mathrm{A}+\delta \mathrm{A}$ ) off-axis vector coordinates
$\Delta O P D=B_{x}[\delta E \sin E \sin \mathrm{~A}-\delta \mathrm{A} \operatorname{cosEcos} \mathrm{A}]-B_{y}[\delta \mathrm{Esin} \mathrm{E} \cos \mathrm{A}+\delta \mathrm{A} \operatorname{cosEsin} \mathrm{A}]$

With $\mathrm{B} \sim 10^{2} \mathrm{~m}$ the second order terms are negligible for $\mathrm{a} \sim 10$ arcmin field

## $\Delta \mathrm{OPD}$ function is a tilted plane



## Equalization of the $\Delta \mathrm{OPD}$

Focal plane

## Staircase Mirror working principle

requirements:
-long focal depth
-small $\Delta \mathrm{OPD} / \mathrm{PSF}$ (Point Spread Function)

- large w/PSF



## Experimental setup



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## Application to VLTI

Calculation of the step depth and rotation angle of the equalization mirror

Input:
-declination and right ascension of the stellar object
$\cdot \mathrm{u}, \mathrm{v}$ site coordinates of the telescopes
Output:
-staircase mirror shape with fixed width and adaptable depth and rotation angle as a function of Local Sidereal Time (LST) for object tracking.

## VLTI parameters

VLTI optical parameters:
-entrance pupil 8,000 mm
-focal length $408,000 \mathrm{~mm}$
-field of view in Coudé focus 2 arcmin diameter
-scale 1.98 mm per arcsec on the sky
${ }^{-} \mathrm{L}=24^{\circ} 38^{\prime} \mathrm{S}$
-Central wavelength $\lambda=2.2 \mu \mathrm{~m}$
-Bandwidth $\Delta \lambda=0.2 \mu \mathrm{~m}$

- Mirror angle $\alpha=\pi / 4 \mathrm{rad}$


## $\Delta$ OPD surface

$$
\begin{gathered}
\text { A (arcsec) } \\
\\
\\
\\
\\
\\
\\
1
\end{gathered}
$$

UT2 $(24,24)$ and UT4 $(112,8)$


## Mirror shape

UT2 $(24,24)$ and UT4 $(112,8)$ $\mathrm{w} \approx 400 \mu \mathrm{~m}$ ( 0.2 arcsec ) $\mathrm{d}_{\max }=30 \mu \mathrm{~m}$


## Conclusions

-Wide FOV of several arcmin can be reached using this technique.
-Shape of the mirror changes with pointing direction. An actuated mirror is needed for earth-based interferometers.
-The w/PSF ratio for the Coudé focus on the VLTI is small (only 2 PSF's per step). It is necessary to decrease the PSF or increase the scale.

## Future work

-Performing a simulation in order to study the effect of the steps on the detected visibility
-Setup implementation and "first fringes"

## System parameters

| $\Theta(\mathrm{rad})$ | 0.00029089 | F4 (mm) | +800 | s ( $\mu \mathrm{m} / \mathrm{arcs}$ ) | 32.46 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| D2 (mm) | 20 | F (mm) | 6563.567 | $\delta(\mu \mathrm{m})$ | 328 |
| B (mm) | 30 | BFL (mm) | 394.22 | d ( $\mu \mathrm{m}$ ) | 1948 |
| F2 (mm) | +1330 | NA | $1.25 \mathrm{e}-3$ | D3 (mm) | 3.047 |
| F2' (mm) | -100 | $\mathbf{Z}_{\mathrm{f}}(\mathrm{mm})$ | 367.214 | b (mm) | 4.571 |
| F2-F2' (mm) | 1258.67 | $\lambda_{0}(\mathrm{~nm})$ | 575 | $\Theta^{\prime}$ (rad) | 0.0019055 |
| F2'-I (mm) | 394.218 | $\delta \lambda(\mathrm{nm})$ | 150 | $\delta^{\prime}(\boldsymbol{\mu m})$ | 151 |
| F2-I (mm) | 1652.888 | $\mathbf{L}_{\mathbf{c}}(\mu \mathrm{m})$ | 2.2 | $\mathbf{d}^{\prime}(\mu \mathrm{m})$ | 1903 |
| F3 (mm) | $+1000$ | m | 6.563 |  |  |

## Spot size vs. wavelength



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## Back focal length vs. wavelength




